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(54) **Polyvinyl chloride resin composition for powder molding and production and use thereof.**

(57) Disclosed herein is a polyvinyl chloride resin composition for powder molding which comprises granular polyvinyl chloride resin (as component A), particulate polyvinyl chloride resin (as component B), stabilizer, plasticizer, and saccharide (as component C). Disclosed also herein is a process for producing said resin composition by mixing granular polyvinyl chloride resin (as component A), particulate polyvinyl chloride resin (as component B), stabilizer, plasticizer, and saccharide (as component C). The resin composition is suitable for the production of covering materials for automotive interior.

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The present invention relates to a polyvinyl chloride resin composition for powder molding and also to producing and using the same.

The recent trend in the automotive interior covering materials for crash pad, armrest, headrest, console box, meter hood, door trim, etc. is towards those which are both lightweight and also soft to the touch and of quality appearance owing to embossing for the leather-like finish and stitch-like pattern.

These covering materials are conventionally produced by the powder slush molding method which consists of contacting a powder composition with a heated mold, thereby causing particles to fuse together, and removing excess powder remaining unfused, said powder composition being formed by dry-blending polyvinyl chloride resin, plasticizer, stabilizer, pigment, etc.

The product of powder slush molding is usually backed with a polyurethane layer to be made into a covering material. The thus obtained covering material has the disadvantage of poor adhesion between the polyvinyl chloride resin layer and the polyurethane layer.

In order to overcome this disadvantage, there has been proposed an improved powder slush molding method which employs a polyvinyl chloride resin composition containing polypropylene glycol or a modified product thereof, i.e., polyether polyol. (Japanese Patent Kokai No. 136542/1986)

This molding method, however, is not satisfactory because the resin composition does not adhere uniformly to the mold or the excess of the resin composition is not removed uniformly after fusing. Thus the resulting molded article fluctuates widely in thickness and has an irregular back surface.

With the foregoing in mind, the present inventors carried out a series of researches which led to the finding that it is possible to produce a covering material which has uniform thickness and good adhesion to the polyurethane layer if the resin composition for powder molding contains saccharide.

According to the present invention, the resin composition contains component A which is a granular polyvinyl chloride resin, such as homopolymers of vinyl chloride, copolymers of vinyl chloride with a copolymerizable monomer (e.g., ethylene, propylene, and vinyl acetate), and graft copolymers of ethylene-vinyl acetate copolymer with vinyl chloride. These examples are not limitative. Two or more polymers may be used in combination with one another.

The granular polyvinyl chloride resin usually has a particle diameter of 100-150 μm . It is usually produced by suspension polymerization or bulk polymerization.

According to the present invention, the resin composition contains component B which is a particulate polyvinyl chloride resin, such as homopolymers of vinyl chloride and copolymers of vinyl chloride with a copolymerizable monomer (e.g., ethylene, propylene, and vinyl acetate). Two or more polymers may be used in combination with one another. Component B is intended to coat the granules A. The weight ratio A/B is preferably 97/3 to 80/20.

The particulate polyvinyl chloride resin usually has a particle diameter of 0.1-10 μm . It is usually produced by emulsion polymerization or micro-suspension polymerization.

According to the present invention, the resin composition contains component C which is saccharide - e.g. of formula $\text{C}_n\text{H}_{2n}\text{O}_n$, where n is an integer of 3-9.

Monosaccharides (such as triose, tetrose, pentose, hexose, heptose, octose, and nonose), sugar alcohols (e.g. reduction products of monosaccharides), oligosaccharides (such as maltose and cyclodextrin), and polysaccharides (such as glycogen) are suitable for C.

Component C is best used in an amount of 0.05-6 parts by weight per 100 parts by weight of components A and B put together.

The polyvinyl chloride resin composition of the present invention may be prepared by dry-blending A with any adjuvants and component C and then incorporating the dry blend with component B, or by dry-blending A with any adjuvants and then incorporating the dry blend with a mixture of components B and C. The dry-blending is usually carried out at 60-130°C and the subsequent incorporation is usually carried out at 40-80°C.

The mixture of components B and C should preferably be prepared by mixing a latex (as a polymerization product) with component C (or an aqueous solution thereof), followed by spray drying. The spray-dried product may be crushed by a microatomizer.

In the case where component C is added by dry-blending, the amount of component C can be e.g. 0.6-6 parts by weight, preferably 1-5 parts by weight, per 100 parts by weight of components A and B put together. In the case where component C is added in the form of mixture with component B, the amount of component C can be e.g. 0.05-0.6 part by weight, preferably 0.1-0.5 part by weight per 100 parts by weight of components A and B put together.

According to the present invention, the resin composition may include optional adjuvants such as blowing agent, blowing auxiliary, filler, and pigment;

plasticizer and stabilizer are usually present.

Suitable plasticizers include dialkyl phthalates with the alkyl group containing 9-11 carbons (such as dii-

sodecyl phthalate and diisoundecyl phthalate), and trialkyl trimellitates with the alkyl group containing 7-11 carbons (such as trioctyl trimellitate, tri-2-ethylhexyl trimellitate, and tridecyl trimellitate). Any other plasticizers can be used which are ordinarily incorporated into resin compositions for powder molding. The plasticizer is usually used in an amounts of 40-120 parts by weight per 100 parts by weight of the polyvinyl chloride resin.

Suitable stabilizers include compounds, particularly carboxylates, of metals such as zinc, barium, sodium, potassium, calcium, lithium, and tin. They should preferably be used in combination with one another. The stabilizer may be used in combination with any of magnesium oxide, magnesium hydroxide, hydrotalcite, zinc oxide, barium oxide, calcium oxide, barium phosphate, and the like. The stabilizer may also be used in combination with antioxidant (derived from phenols, thioethers, phosphites, etc.), light stabilizer (derived from diketo compounds, salicylic acid, benzophenone, benzotriazole, etc.), and epoxy compound. They are not specifically limited so long as they are selected from those which can be used for resin compositions for powder molding. The stabilizer is usually used in an amount of 3-15 parts by weight per 100 parts by weight of the polyvinyl chloride resin.

Suitable blowing agents include the thermal decomposition type, such as azodicarbonamide, p,p'-oxybis-benzenesulfonylhydrazide, p-toluenesulfonylhydrazide, and benzenesulfonylhydrazide, of which the first one is most desirable. They may be used in combination with one another.

The blowing agent is usually used in an amount of 1-10 parts by weight per 100 parts by weight of the polyvinyl chloride resin.

The blowing agent may be used in combination with a blowing auxiliary, e.g. one or more of zinc oxide, inorganic zinc salt (such as zinc nitrate), zinc fatty acid soap (such as zinc octoate and zinc stearate), and urea. The blowing auxiliary is usually used in an amount of 0.2-3 parts by weight per 100 parts by weight of the polyvinyl chloride resin.

The invention has been described in its general form. The polyvinyl chloride resin composition of the invention offers the advantage of forming a uniform layer on the mold surface, permitting the smooth removal of excess powder from the mold. The resulting molded article has good adhesion to a polyurethane layer when it is made into a covering material in a subsequent process.

EXAMPLES

To further illustrate the invention, and not by way of limitation, the following examples are given. (Non-foamable resin composition for powder molding)

Example 1

(Preparation of resin composition)

A supermixer was charged with 90 parts by weight of granular polyvinyl chloride resin (produced by suspension polymerization, having an average particle diameter of 120 μm and an average degree of polymerization of 800). After heating to 80°C with uniform stirring, the resin was dry-blended with 70 parts by weight of trimellitic ester plasticizer, 3 parts by weight of Ba-Zn stabilizer, and 2 parts by weight of sorbitol. Mixing was continued until the temperature of the mixture reached 125°C. Then the mixture was cooled to 50°C. The mixture was uniformly mixed with 10 parts by weight of particulate polyvinyl chloride resin (prepared by micro-suspension polymerization, having an average particle diameter of 1 μm and an average degree of polymerization of 1300). Thus there was obtained a non-foamable resin composition for powder molding.

(Preparation of single-layer sheet)

The non-foamable resin composition was sprinkled over a nickel flat mold which had just been removed from a Geer oven at 280°C after preheating to 240°C for 10 minutes. About 13 seconds later, excess powder (remaining unused) was removed, and the mold was heated again in a Geer oven at 240°C for 1 minute. After cooling, the layer of the resin composition was released from the mold. Thus there was obtained a molded sheet

The resin composition was evaluated as follows. The results are shown in Table 1.

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(Method of evaluation)

(1) Removability of excess powder

- 5 . Evaluated by observing the back of the molded sheet. The resin composition is rated as "good" if it gives rise to a molded sheet of uniform thickness and adheres to the mold uniformly.
The resin composition is rated as "poor" if it gives rise to a molded sheet of uneven thickness and adheres to the mold unevenly.
- 10 . Evaluated by filling the resin composition (level, about 75 g) into an aluminum cup (73 mm in inside diameter and 25 mm high), heating the cup on a hot plate at 240°C for 2 minutes, upsetting the aluminum cup, and measuring the amount of the resin composition remaining in the aluminum cup.

(2) Adhesion of the single-layer sheet to semirigid polyurethane resin

- 15 Evaluated by ageing the single-layer sheet at 50°C and 50% RH for 7 days, backing the single-layer sheet with an approximately 10 mm thick layer of semirigid polyurethane resin in a polyurethane foaming mold, cutting a 25mm wide test piece out of the sample, and measuring the 180° peel strength between the layer of the polyvinyl chloride resin and the layer of the semirigid polyurethane resin.
- 20 . The molding composition is rated as "good" if peeling occurs in the material (which indicates good adhesion at the interface).
. The molding composition is rated as "poor" if peeling occurs at the interface (which indicates poor adhesion at the interface).

Examples 2 and 3 and Comparative Examples 1 and 2

25 (Preparation of resin compositions)

Resin compositions were prepared in the same manner as in Example 1 except that the amount of sorbitol was changed as shown in Table 1.

30 (Preparation of single-layer sheets)

Each of the resin compositions was made into a single-layer sheet in the same manner as in Example 1. The results of evaluation are shown in Table 1.

35 Table 1

	Example No.			Comparative Example No.	
	1	2	3	1	2
40 Sorbitol (pbw)	2	1	5	0	7
Adhesion	good	good	good	poor	good
45 Removability of excess powder					
Back of sheet	good	good	good	good	poor
Amount adhering to cup (g)	25.6 (A)	25.5 (A)	26.1 (A)	24.8 (B)	27.7 (A)
50 Difference between (A) and (B), (g)	0.8	0.7	1.3	0	2.9

55 Example 4

The same procedure as in Example 1 was repeated except that the resin composition was prepared with

2 parts by weight of mannitol in place of sorbitol. The resulting molded sheet exhibited good adhesion to the polyurethane layer. The amount of powder adhering to the cup was 25.3 g (which is larger than that in Comparative Example 1 by 0.5 g). The back of the molded sheet showed no sign of uneven thickness.

5 Example 5

The same procedure as in Example 1 was repeated except that the resin composition was prepared with 2 parts by weight of glucose in place of sorbitol. The resulting molded sheet exhibited good adhesion to the polyurethane layer. The amount of powder adhering to the cup was 25.5 g (which is larger than that in Comparative Example 1 by 0.7 g). The back of the molded sheet showed no sign of uneven thickness.

Comparative Example 3

The same procedure as in Example 1 was repeated except that the resin composition was prepared with 2 parts by weight of polypropylene glycol in place of sorbitol. The resulting molded sheet exhibited good adhesion to the polyurethane layer. The amount of powder adhering to the cup was 31.8 g (which is larger than that in Comparative Example 1 by 6.8 g). The back of the molded sheet showed signs of uneven thickness.

Comparative Example 4

The same procedure as in Example 1 was repeated except that the resin composition was prepared with 2 parts by weight of polyether polyol (Sumiphen 3063 made by Sumitomo Bayer Urethane Co., Ltd.) in place of sorbitol. The resulting molded sheet exhibited good adhesion to the polyurethane layer. The amount of powder adhering to the cup was 35.7 g (which is larger than that in Comparative Example 1 by 10.7 g). The back of the molded sheet showed signs of uneven thickness.

Example 6

(Preparation of saccharide-containing particulate polyvinyl chloride resin)

A 100-liter autoclave with glass lining was charged with 40 kg of deionized water and 920 g of polyvinyl chloride in the form of latex having an average particle diameter of 0.3 μm . The atmosphere in the autoclave was replaced with nitrogen under reduced pressure. The autoclave was further charged with 34 kg of vinyl chloride monomer. The autoclave was heated to start polymerization. Throughout the period of polymerization, hydrogen peroxide in a total amount of 0.004 wt% (of the amount of vinyl chloride monomer) and Rongalite in a total amount of 1.0 equivalent mol (with respect to hydrogen peroxide) were introduced into the autoclave at a constant rate through separate inlets. After the rate of polymerization had reached 12%, sodium lauryl sulfate (as an emulsifier) was continuously added to the autoclave at a ratio of 0.03% (of the amount of vinyl chloride monomer) every hour until polymerization was complete. Polymerization was suspended when the polymerization pressure decreased by 1 kg/cm² from the saturated vapor pressure of vinyl chloride at the polymerization temperature, and unreacted monomer was recovered. The amount of sodium lauryl sulfate added was 0.3 wt% of the amount of polymer produced, and the average particle diameter of the polymer was 1.0 μm .

The thus obtained latex (containing 3 kg of polyvinyl chloride resin) was mixed with an aqueous solution prepared by dissolving 150 g of sorbitol in hot water at 80°C. Then the latex was adjusted to pH 7 with sodium carbonate.

Finally, the latex was spray-dried at a rate of 37 g/min using a rotational disc atomizer (12 cm in diameter), with the inlet temperature and outlet temperature kept at 160°C and 60°C, respectively. The dried product was crushed using a microatomizer. Thus there was obtained a white powder.

(The above-mentioned procedure was used in the following example for the production of saccharide-containing particulate vinyl chloride resin.)

(Preparation of resin composition)

A supermixer was charged with 90 parts by weight of granular polyvinyl chloride resin (produced by suspension polymerization, having an average particle diameter of 120 μm and an average degree of polymerization of 800). After heating to 80°C with uniform stirring, the resin was dry-blended with 70 parts by weight of trimellitic ester plasticizer and 3 parts by weight of Ba-Zn stabilizer. Mixing was continued until the temper-

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ature of the mixture reached 125°C. Then the mixture was cooled to 50°C. The mixture was uniformly mixed with 10 parts by weight of the particulate polyvinyl chloride resin prepared as mentioned above. Thus there was obtained a non-foamable resin composition for powder molding.

5 (Preparation of single-layer sheet)

The non-foamable resin composition was sprinkled over a nickel flat mold which had just been removed from a Geer oven at 280°C after preheating to 240°C for 10 minutes. About 13 seconds later, excess powder (remaining unfused) was removed, and the mold was heated again in a Geer oven at 240°C for 1 minute. After cooling, the layer of the resin composition was released from the mold. Thus there was obtained a molded sheet. The results of evaluation are shown in Table 2.

Examples 7 and 8 and Comparative Examples 5 and 6

15 (Preparation of resin compositions)

Resin compositions were prepared in the same manner as in Example 6 except that the amount of sorbitol was changed to 30, 120, 0, and 300 g, respectively.

20 (Preparation of single-layer sheets)

Each of the resin compositions was made into a single-layer sheet in the same manner as in Example 6. The results of evaluation are shown in Table 2.

Table 2

	Example No.			Comparative Example No.	
	6	7	8	5	6
30 Sorbitol (pbw)	0.5	0.1	0.4	0	1.0
Adhesion	good	good	good	poor	good
Removability of excess powder					
35 Back of sheet	good	good	good	good	poor
Amount adhering to cup (g)	26.3 (A)	25.9 (A)	26.5 (A)	25.0 (B)	28.1 (A)
40 Difference between (A) and (B), (g)	1.3	0.9	1.5	0	3.1

Example 9

The same procedure as in Example 6 was repeated except that the resin composition was prepared with 60 g by weight of mannitol in place of sorbitol. The resulting molded sheet exhibited good adhesion to the polyurethane layer. The amount of powder adhering to the cup was 25.6 g (which is larger than that in Comparative Example 5 by 0.6 g). The back of the molded sheet showed no sign of uneven thickness.

Example 10

The same procedure as in Example 6 was repeated except that the resin composition was prepared with 60 g by weight of glucose in place of sorbitol. The resulting molded sheet exhibited good adhesion to the polyurethane layer. The amount of powder adhering to the cup was 26.0 g (which is larger than that in Comparative Example 5 by 1.0 g). The back of the molded sheet showed no sign of uneven thickness.

(Foamable resin composition for powder molding)

Example 11

5 (Preparation of foamable resin composition)

A supermixer was charged with 90 parts by weight of granular polyvinyl chloride resin (produced by suspension polymerization, having an average particle diameter of 120 μm and an average degree of polymerization of 800). After heating to 80°C with uniform stirring, the resin was dry-blended with 70 parts by weight of trimellitic ester plasticizer, 3 parts by weight of Ba-Zn stabilizer, 1.5 parts by weight of azodicarbonamide, 1 part by weight of zinc oxide, and 2 parts by weight of sorbitol. Mixing was continued until the temperature of the mixture reached 125°C. Then the mixture was cooled to 50°C. The mixture was uniformly mixed with 10 parts by weight of particulate polyvinyl chloride resin (prepared by microsuspension polymerization, having an average particle diameter of 1 μm and an average degree of polymerization of 1300). Thus there was obtained a foamable resin composition for powder molding.

(Preparation of double-layer sheet from the non-foamable resin composition and the foamable resin composition)

20 The sorbitol-free non-foamable resin composition (prepared in Comparative Example 1) was sprinkled over a nickel flat mold which had just been removed from a Geer oven at 280°C after preheating to 240°C for 10 minutes. About 5 seconds later, excess powder (remaining unfused) was removed. The foamable resin composition was sprinkled over the mold. About 15 seconds later, excess powder (remaining unfused) was removed, and the mold was heated again in a Geer oven at 240°C for 1 minute so as to effect foaming. After cooling, the double-layer of the resin composition was released from the mold. The results of evaluation of the double-layer sheet are shown in Table 3.

(Method of evaluation)

30 (1) Adhesion of the double-layer sheet to semirigid polyurethane resin

Evaluated by ageing the double-layer sheet at 25°C and 50% RH for 1 day, backing the double-layer sheet with an approximately 10 mm thick layer of semirigid polyurethane resin in a polyurethane foaming mold, cutting a 25mm wide test piece out of the sample, and measuring the 180° peel strength between the layer of the polyvinyl chloride resin and the layer of the semirigid polyurethane resin. (The 180° peel strength was measured at 23°C and at a pulling rate of 200 mm/min.)

Evaluation of other items was carried out in the same manner as in Example 1.

Examples 12 and 13 and Comparative Examples 7 and 8

40

(Preparation of foamable resin compositions)

Foamable resin compositions were prepared in the same manner as in Example 11 except that the amount of sorbitol was changed as shown in Table 3.

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(Preparation of double-layer sheets)

Each of the foamable resin compositions was made into a double-layer sheet in the same manner as in Example 11. The results of evaluation are shown in Table 3.

50

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Table 3

	Example No.			Comparative Example No.	
	11	12	13	7	8
Sorbitol (pbw)	2	1	5	0	7
Peel strength, kg/25 mm	0.55	0.45	0.65	0.20	0.70
Removability of excess powder					
Back of sheet	good	good	good	good	poor
Amount adhering to cup (g)	26.1 (A)	25.7 (A)	26.5 (A)	25.0 (B)	28.0 (A)
Difference between (A) and (B), (g)	1.1	0.7	1.5	0	3.0

Example 14

The same procedure as in Example 11 was repeated except that the foamable resin composition was prepared with 2 parts by weight of mannitol in place of sorbitol. The peel strength between the double-layer sheet and the polyurethane layer was 0.55 kg/25 mm. The amount of powder adhering to the cup was 25.6 g (which is larger than that in Comparative Example 7 by 0.6 g). The back of the molded sheet showed no sign of uneven thickness.

Example 15

The same procedure as in Example 11 was repeated except that the foamable resin composition was prepared with 2 parts by weight of glucose in place of sorbitol. The peel strength between the double-layer sheet and the polyurethane layer was 0.50 kg/25 mm. The amount of powder adhering to the cup was 26.0 g (which is larger than that in Comparative Example 7 by 1.0 g). The back of the molded sheet showed no sign of uneven thickness.

Comparative Example 9

The same procedure as in Example 11 was repeated except that the foamable resin composition was prepared with 2 parts by weight of propylene glycol in place of sorbitol. The peel strength between the double-layer sheet and the polyurethane layer was 0.40 kg/25 mm. The amount of powder adhering to the cup was 32.1 g (which is larger than that in Comparative Example 7 by 7.1 g). The back of the molded sheet showed signs of uneven thickness.

Comparative Example 10

The same procedure as in Example 11 was repeated except that the foamable resin composition was prepared with 2 parts by weight of polyether polyol in place of sorbitol. The peel strength between the double-layer sheet and the polyurethane layer was 0.30 kg/25 mm. The amount of powder adhering to the cup was 35.8 g (which is larger than that in Comparative Example 7 by 10.8 g). The back of the molded sheet showed signs of uneven thickness.

Example 16

(Preparation of foamable resin composition)

A supermixer was charged with 90 parts by weight of granular polyvinyl chloride resin (produced by sus-

pension polymerization, having an average particle diameter of 120 μm and an average degree of polymerization of 800). After heating to 80°C with uniform stirring, the resin was dry-blended with 70 parts by weight of trimellitic ester plasticizer, 3 parts by weight of Ba-Zn stabilizer, 1.5 parts by weight of azodicarbonamide, and 1.5 parts by weight of zinc oxide. Mixing was continued until the temperature of the mixture reached 125°C. Then the mixture was cooled to 50°C. The mixture was uniformly mixed ; with 10 parts by weight of particulate polyvinyl chloride resin (prepared by microsuspension polymerization, having an average particle diameter of 1 μm and an average degree of polymerization of 1300) which contains 2 parts by weight of sorbitol for 100 parts by weight of the particulate polyvinyl chloride resin. Thus there was obtained a foamable resin composition for powder molding.

(Preparation of double-layer sheet from the non-foamable resin composition and the foamable resin composition)

The sorbitol-free non-foamable resin composition (prepared in Comparative Example 1) was sprinkled over a nickel flat mold which had just been removed from a Geer oven at 280°C after preheating to 240°C for 10 minutes. About 5 seconds later, excess powder (remaining unfused) was removed. The foamable resin composition was sprinkled over the mold. About 15 seconds later, excess powder (remaining unfused) was removed, and the mold was heated again in a Geer oven at 240°C for 1 minute so as to effect foaming. After cooling, the double-layer of the resin composition was released from the mold. The results of evaluation of the double-layer sheet are shown in Table 4.

Examples 17 and 18 and Comparative Examples 11 and 12

(Preparation of foamable resin compositions)

Foamable resin compositions were prepared in the same manner as in Example 16 except that the particulate polyvinyl chloride resin was replaced by the one which contains sorbitol in an amount of 1, 4, 0, and 10 parts by weight, respectively, for 100 parts by weight of the particulate polyvinyl chloride resin.

(Preparation of double-layer sheets)

Each of the foamable resin compositions was made into a double-layer sheet in the same manner as in Example 16. The results of evaluation are shown in Table 4.

Table 4

	Example No.			Comparative Example No.	
	16	17	18	11	12
Sorbitol (pbw)	0.2	0.1	0.4	0	1.0
Peel strength, kg/25 mm	0.65	0.55	0.75	0.20	0.90
Removability of excess powder					
Back of sheet	good	good	good	good	poor
Amount adhering to cup (g)	26.5 (A)	26.1 (A)	26.1 (A)	25.0 (B)	28.1 (A)
Difference between (A) and (B), (g)	1.5	1.1	1.3	0	3.1

Example 19

The same procedure as in Example 16 was repeated except that the particulate polyvinyl chloride resin was replaced by the one which contains 2 parts by weight of mannitol for 100 parts by weight of particulate

polyvinyl chloride resin. The peel strength between the double-layer sheet and the polyurethane layer was 0.65 kg/25 mm. The amount of powder adhering to the cup was 26.2 g (which is larger than that in Comparative Example 11 by 1.2 g). The back of the molded sheet showed no sign of uneven thickness.

5 Example 20

10 The same procedure as in Example 16 was repeated except that the particulate polyvinyl chloride resin was replaced by the one which contains 2 parts by weight of glucose for 100 parts by weight of particulate polyvinyl chloride resin. The peel strength between the double-layer sheet and the polyurethane layer was 0.60 kg/25 mm. The amount of powder adhering to the cup was 25.5 g (which is larger than that in Comparative Example 11 by 1.5 g). The back of the molded sheet showed no sign of uneven thickness.

Claims

- 15 1. A polyvinyl chloride resin powder molding composition which comprises granular polyvinyl chloride resin (component A), particulate polyvinyl chloride resin (component B), and saccharide (component C).
- 20 2. A composition according to claim 1, wherein the ratio of component B to component A is from 3/97 to 20/80 by weight.
3. A composition according to claim 1 or 2, wherein the amount of component C is 0.05-6 parts by weight per 100 parts by weight of components A and B put together.
- 25 4. A composition according to claim 1 or 2 or 3, which contains one or more of stabilizer, plasticizer and blowing agent.
- 30 5. A process for producing a polyvinyl chloride resin powder molding composition comprising mixing granular polyvinyl chloride resin (component A), particulate polyvinyl chloride resin (component B), saccharide (component C), and optionally stabilizer and plasticizer.
6. A process according to claim 5, which comprises dry-blending components A and C and optionally one or more of stabilizer, plasticizer, and optional blowing agent, and subsequently mixing the dry blend with component B.
- 35 7. A process according to claim 6, wherein the amount the component C is 0.6-6 parts by weight per 100 parts by weight of components A and B put together.
8. A process according to claim 5, which comprises mixing components B and C, and mixing the resulting combination with component A (optionally dry-blended with one or more of stabilizer, plasticizer, and blowing agent).
- 40 9. A process according to claim 8, wherein the amount of component C is 0.05-0.6 parts by weight per 100 parts by weight of components A and B put together.
- 45 10. A process for producing a covering material, said process comprising powder-molding a composition which is according to any of claims 1 to 4 or which is obtainable by a process according to any of claims 5 to 9.

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European Patent
Office

EUROPEAN SEARCH REPORT

Application Number

EP 92 30 9493

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
X	JP-A-1 156 357 (HITACHI CHEM. KK) * example 2 * -----	1	C08L27/06 C08J3/22 //C08L27/06, C08L27:06)
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			C08L C08J C08K
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 18 JANUARY 1993	Examiner Dieter Schuler
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document</p>			

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